

CURE CHARACTERISTICS AND CROSSLINK DENSITY OF NATURAL RUBBER/STYRENE BUTADIENE RUBBER BLENDS

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Abstract

By using a semi-efficient vulcanization system, the cure characteristics and crosslink density of natural rubber/styrene butadiene rubber (NR/SBR) blends were studied with a blend ratio from 0 to 100% rubber. The scorch time, optimum cure time, and torque difference value of the blended rubber compounds were determined by using the Moving-Die Rheometer (MDR 2000). The crosslink density was determined by the Flory—Rehner approach. Results indicate that the scorch and cure times, ts_2 and t_{90} , of the NR/SBR blends increased with increasing the SBR content. Whilst, the maximum values of torque difference and crosslink density were performed by the NR/SBR blend with a blend ratio of 75/25.

Keywords : Natural Rubber; Styrene Butadiene Rubber; Scorch time; Cure time; Torque difference, Crosslink density.

Abstrak :

Dengan menggunakan sistim vulkanisasi semi-efisien, karakteristik pematangan dan kerapatan sambung silang dari kompon adonan-adonan Karet Alam/Karet Stirena Butadiena (KA/KSB) diamati. Rasio adonan adalah dari 0% ke 100% karet. Waktu skorj, waktu pematangan optimum, dan selisih tork dari adonan-adonan karet tersebut ditentukan dengan menggunakan Moving-Die Rheometer (MDR 2000). Kerapatan sambung silang diukur dengan menggunakan metode Flory - Rehner. Hasil pengamatan menunjukkan bahwa waktu skorj dan waktu pematangan optimum, ts_2 and t_{90} , meningkat dengan meningkatkan komposisi KSN di dalam adonan karet-karet tersebut. Nilai-nilai selisih tork dan kerapatan sambung silang yang maksimum diperoleh oleh adonan KA/KSB dengan rasio adonan 75/25.

Kata kunci : Karet Alam; Karet Stirena Butadiena; Waktu skorj; Waktu pematangan optimum; Kerapatan sambung silang.

Introduction

In rubber technology, blending of some raw rubbers is an attempt to produce some new rubbery materials with a wide range of applications. The attempt takes some advantages of the attractive properties of the blend constituents while avoiding the economical and technical uncertainties associated with synthesising new rubbery materials [6,13]. The blending of two or more raw rubbers of different types is useful for the preparation of materials with properties absent in the rubber components [9,11,14]. Natural rubber (NR) and its blended compounds have been extensively studied because of their superior performance in a wide range of applications, especially in tire application. Natural rubber is prone to deterioration by ozone attack due to its highly unsaturated polymeric backbone. In general, improvement in the poor ozone resistance of NR can be achieved by blending it with low-unsaturation rubbers such as styrene butadiene rubber (SBR). SBR is obtained by polymerising

styrene and butadiene with a relatively small amount of a non-conjugated diene, which usually imparts good resistance to aging, weathering and chemical resistance [1,3,6].

In this study, NR was blended with SBR with some of blend ratios. The cure characteristics and crosslink density of blended NR/SBR compounds were studied. Cure characteristics of the blended rubber compounds were determined by using a Moving Die Rheometer which cured at 150 °C, with, and the crosslink density was measured by the Flory—Rehner approach.

Experimental

Materials

Natural Rubber, and Styrene Butadiene Rubber were used. Other compounding ingredients were sulphur, zinc oxide, stearic acid,

N-isopropyl-N'-phenyl-p-phenylenediamine (IPPD), N-sikloheksil-2-benzol tiazolsulfenamide (CBS).

Compounding

A semi efficient vulcanization system was used for compounding. The recipe for the preparation of the NR/SBR blended compound is given in Table 1. The compounding procedure was done in accordance with the American Society for Testing and Material (ASTM) – Designation D 3184 – 80. Compounding was done on two-roll mill.

Table 1. A typical formulation of the blended rubber compounds

Ingredients	Content (phr) ^a
Rubber blend ^b	100.0
Zinc oxide	5.0
Stearic acid	2.0
IPPD	2.0
CBS	1.5
Sulphur	1.5

^a parts per hundred parts of rubber

^b Blend ratio for NR/SBR (100/0, 75/25, 50/50, 25/75, and 0/100).

Cure Characteristics

The cure characteristics of the NR/SBR blended compounds were obtained using a Monsanto Moving Die Rheometer (MDR 2000), which was employed to determine the scorch time (t_{s2}), cure time (t_{90}) and torque difference ($M_H - M_L$), according to ISO 3417. Samples of the respective compounds were tested at 150°C. The compounds were subsequently compression-moulded using a stainless steel mould at 150°C, with a pressure of 10 MPa, and applying a laboratory hot-press based on respective curing times.

Measurement of crosslink density

Swelling tests on the rubber vulcanisates were performed in toluene in accordance with ISO 1817. The cured test pieces (30 mm × 5 mm × 2 mm) were weighed using an electrical balance and swollen in toluene until equilibrium, which took 72 hours at room temperature. The samples were taken out from the liquid, the toluene was removed from the sample surfaces and the weight was determined. The samples were then dried in

the oven at 60°C until constant weights were obtained. The swelling results were used to calculate the molecular weight between two crosslinks (M_c) by applying the Flory-Rehner Equation [8].

$$M_c = \frac{-\rho_p V_s V_r^{1/3}}{\ln(1 - V_r) + V_r + \chi V_r^2} \quad (1)$$

$$V_r = \frac{1}{1 + Q_m} \quad (2)$$

where ρ is the rubber density (ρ of NR = 0.92 g/cm³), V_s is the molar volume of the toluene ($V_s = 106.4$ cm³/mol), V_r is the volume fraction of the polymer in the swollen specimen, Q_m is the weight increase of the blends in toluene and χ is the interaction parameter of the rubber network-solvent (χ of NR = 0.393). The degree of the crosslink density is given by;

$$V_c = \frac{1}{2M_c} \quad (3)$$

Results And Discussion

The cure characteristics

The scorch and cure times of NR/SBR blends are shown in Figure 1. The scorch and cure times of NR/SBR blended compounds increased with increasing the content of SBR in the rubber blends. According to Chouch and Chang [7,12], the cure rate of a rubber compound depends on the number of allylic hydrogen atoms in the statistical repeat unit, whereby a higher content of allylic hydrogen resulted in a lower overall apparent activation energy of curing, thus increasing the speed of the cure rate. Therefore, longer scorch and cure times were attributed to a lower allylic hydrogen content of the blended rubber compounds. Generally, a statistical repeated unit of NR and SBR have 7 and 3.3 allylic hydrogen atoms, respectively [12].

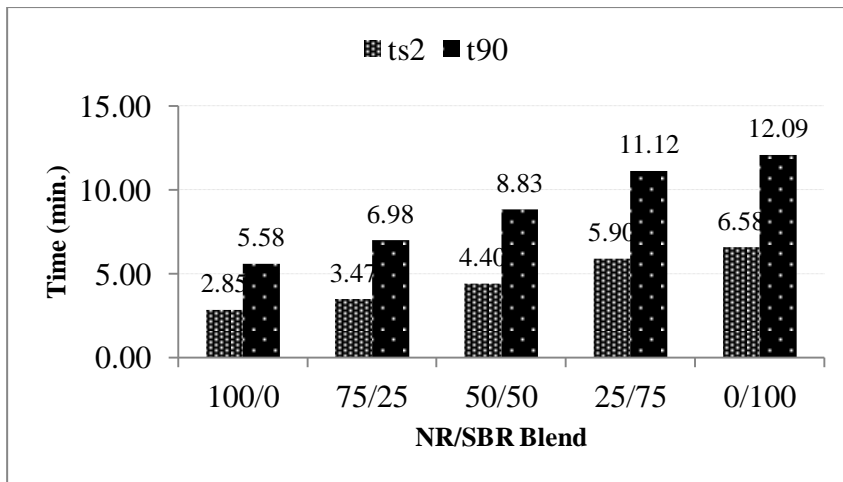


Figure 1. Scorch and cure times of NR/SBR blended compound

Figure 2 shows the torque difference ($M_H - M_L$) of the NR/SBR blended compounds. A 75/25 NR/SBR blended

compound has the highest value of torque difference.

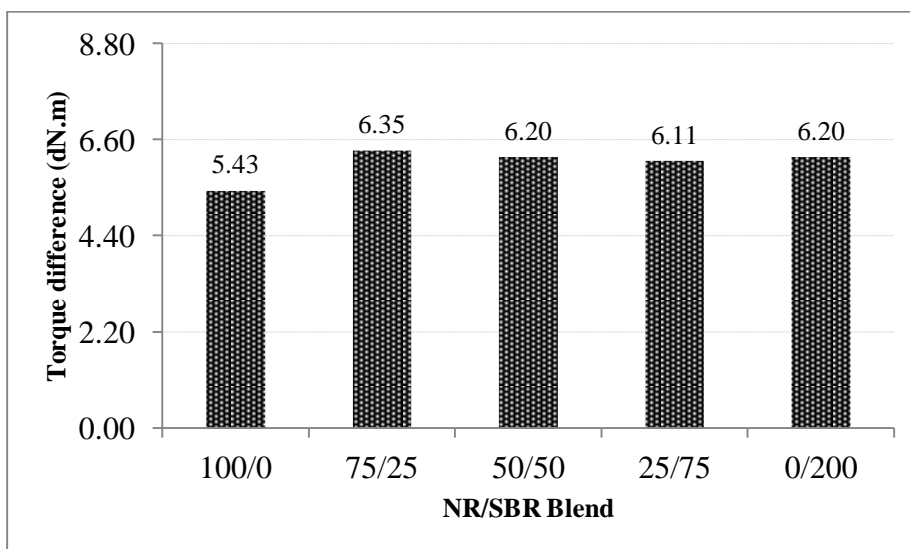


Figure 2. Torque difference of NR/SBR blended compound

The crosslink density

The crosslink densities of the vulcanisates NR/SBR blend were determined by the Flory—Rehner approach [Eq. (1)]. Figure 3 shows the crosslink density of the rubber blended vulcanisates at room temperature. The 75/25 NR/SBR blended rubber compound has the highest degree of crosslink. It can be attributed to the synergetic effect of both raw rubbers, NR and SBR. This

result is in line with Figure 2. The 75/25 NR/SBR blended rubber compound exhibited the highest value of torque difference. Based on theory, torque difference indicates the degree of crosslink density of a rubber compound [2,4,5,10]. The greater the value, the higher is the crosslink density.

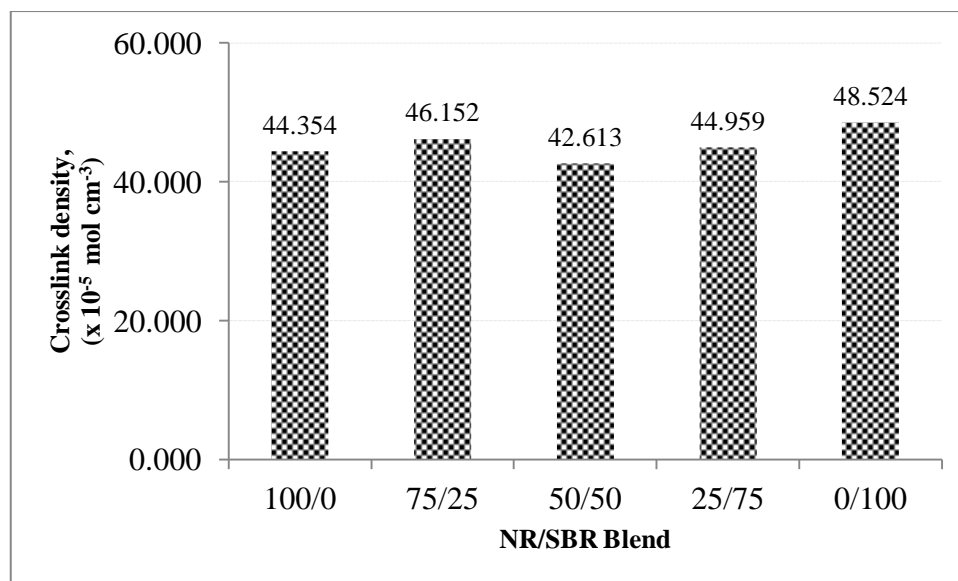


Figure 3. Crosslink density of NR/SBR blended vulcanisate

Conclusions

From this study, the following conclusions can be drawn:

1. The scorch and cure times of natural rubber/styrene butadiene blended compound increase with increasing the content of styrene butadiene rubber.
2. A 75/25 blend ratio is the optimum blend ratio of natural rubber/styrene butadiene rubber blend which produced the maximum values of torque difference and crosslink density.

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